# Tungsten Bronze-Type Solid Solutions $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}$ ( $x=0.3,0.5,0.67,0.71$ ) with Superstructure 

H. Okudera, ${ }^{1}$ H. Nakamura, H. Toraya, and H. Ohsato*<br>Ceramics Research Laboratory, Nagoya Institute of Technology, Asahigaoka 10-6-29, Tajimi 507-0071, Japan;<br>*Department of Materials Science and Engineering, Nagoya Institute of Technology, Gokiso-cho, Showa-ku, Nagoya 466-8555, Japan

Received May 27, 1998; accepted September 14, 1998


#### Abstract

Structural parameters of tungsten bronze-type compounds $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}(x=0.3,0.5,0.67$, and 0.71$)$ were refined in a space group Pbnm by the Rietveld method using highresolution synchrotron radiation powder diffraction data. All the specimens crystallized in the orthorhombic system with a superstructure having the doubled $c$ axis of the reported orthorhombic tungsten bronze-type structure. Unit-cell parameters (in A) are $a=12.1715(5), b=22.3772(3), c=7.67523(9)$ for $x=0.3$, $a=12.1568(1), \quad b=22.3253(2), \quad c=7.66301(7)$ for $x=0.5$, $a=12.1472(1), b=22.2972(2), c=7.65338(6)$ for $x=0.67$, and $a=12.1452(1), b=22.3029(2), c=7.65007(6)$ for $x=0.71$, and $Z=2$. The use of two wavelengths allowed the determination of cation and vacancy distributions over two pentagonal and five tetragonal tunnels in the structure. In the compounds with $x=0.3$ and 0.5 , pentagonal tunnel sites were fully occupied by Ba , and the remaining Ba partially substituted Sm at two of five tetragonal tunnel sites. No evidence was found for the substitution of Sm for Ba at the pentagonal sites, and thus vacancies were formed at the pentagonal sites for $\boldsymbol{x}=0.71$. An amplitude of periodic modulation along the $c$ axis, which caused superstructure, was increased with increasing $x$ in the compositional range examined. A relationship between observed and calculated intensities of superstructure reflections suggests the presence of local lattice distortion, which takes its minimum at $x=0.67$.


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## INTRODUCTION

Physical properties of $\mathrm{Ba}_{6-3 x} R_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}(R=\mathrm{La}$, Nd , and Sm ) series have been investigated for their device applications related to their excellent dielectric properties (1-4). Matveeva et al. (1) reported that $\mathrm{Ba}_{3.75} \mathrm{Pr}_{9.5} \mathrm{Ti}_{18} \mathrm{O}_{54}$ $(x=0.75)$ crystallized in an orthorhombic system. Although the presence of a superstructure doubling the $c$ axis was found, they refined structural parameters by assuming an average cell with a noncentrosymmetric space group Pba2

[^0](No. 32). On the other hand, Ohsato et al. (2) confirmed the formation of solid solutions for $R=\mathrm{Sm}$ over the composition range $0.3 \leq x \leq 0.7$ and refined the structural parameters in a centrosymmetric space group Pbam (No. 55). The basic structure, assumed in these refinements, is a tungsten bronze-type framework structure formed by $\mathrm{TiO}_{6}$ octahedra sharing all apices with each other, and is characterized by distorted tetragonal and pentagonal tunnels running parallel to the $c$ axis. The structure with the noncentrosymmetric space group can be derived by introducing slight displacements of atoms along the $c$ axis in the centrosymmetric space group and both have basically the same atomic arrangement. The superstructure doubling the $c$ axis of the average structure has been also reported for Sm with $x=0.75$ (5). The space group of this structure is either $\mathrm{Pbn}_{1}$ (No. 33) or $\operatorname{Pbnm}$ (No. 62) (5). Recent reinvestigations of the solid solutions for $R=\mathrm{Sm}$ suggested the presence of a superstructure even for $x=0.5$ and $0.71(6,7)$. If the structure belongs to the centrosymmetric space group Pbnm, there should be five crystallographically independent tetragonal tunnel sites [designated by using symbols $\mathrm{A}_{1}(1)$ to $\left.\mathrm{A}_{1}(5)\right]$ and two pentagonal tunnel sites [ $\mathrm{A}_{2}(1)$ and $\left.\mathrm{A}_{2}(2)\right]$ in a unit cell. However, distributions of cations and vacancies over these seven crystallographic sites have not yet been determined.

In the $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}$ system, Sm is expected to be located in the perovskite-like tetragonal cavity ( $\mathrm{A}_{1}$ site) and larger Ba in the pentagonal cavity ( $\mathrm{A}_{2}$ site): a scheme of cation distribution in this system has been proposed as

$$
\begin{align*}
& \left(\mathrm{Sm}_{8+2 x} \mathrm{Ba}_{2-3 x} \square_{x}\right)\left[\mathrm{Ba}_{4}\right] \mathrm{Ti}_{18} \mathrm{O}_{54} \quad(x<2 / 3) \\
& \left(\mathrm{Sm}_{8+2 x} \square_{x}\right)\left[\mathrm{Ba}_{6-3 x} \square_{3 x-2}\right] \mathrm{Ti}_{18} \mathrm{O}_{54}(x \geq 2 / 3), \tag{1}
\end{align*}
$$

where parentheses and square brackets designate $A_{1}$ and $\mathrm{A}_{2}$ sites, respectively, and open squares designate vacancy (8). As can be seen in Eq. [1], this system has a distinctive point at $x=2 / 3$ with respect to cation distribution. Substitution of Sm with Ba at the $\mathrm{A}_{1}$ site in $x<2 / 3$ and the formation of vacancy at the $A_{2}$ site in $x>2 / 3$ have been
ascribed to the occurrence of nonlinear change in dielectric properties at its best with $x=0.6$ (8).

In the present study, the structures of title compounds were analyzed in order to determine the distribution of cations and vacancies over tetragonal and pentagonal tunnel sites. The relationship between the physical property and the modulated local lattice distortion of the framework is discussed.

## EXPERIMENTAL

## Specimens

Pale-yellow sintered materials of $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}$ with $x=0.3,0.5,0.67$, and 0.71 (hereafter abbreviated as BST30, BST50, BST67, and BST71, respectively) were synthesized by solid-state reaction of high-purity reagent chemicals of $\mathrm{BaCO}_{3}(99.7 \%), \mathrm{TiO}_{2}(99.9 \%)$, and $\mathrm{Sm}_{2} \mathrm{O}_{3}$ $(99.9 \%)$ mixed to attain desired compositions. They were ground into powders and used in the following experiments. Scanning-electron microscopic observations showed that individual particles had no apparent morphology corresponding to crystal habit. See Ohsato et al. (3) for more details.

## Intensity Measurement

Powder diffraction experiments using synchrotron radiation were performed with a multiple-detector-system
(MDS) (9) at the $\mathrm{BL}-4 \mathrm{~B}_{2}$ experimental station in the Photon Factory, Tsukuba. Diffracted intensities were measured with two wavelengths of 1.2 and $1.6 \AA(1.54 \AA$ for BST67) at each specimen. The wavelength calibration for monochromatic beam were made by using XANES spectra of $\mathrm{Fe}, \mathrm{Ni}, \mathrm{Au}, \mathrm{Zn}$, and Zr foils, and derived wavelengths were further confirmed using 10 peak positions of the NIST SRM 640b Si powder. Intensity measurements were performed at room temperature in asymmetric $2 \theta$ step scan mode at a fixed incident angle of $8^{\circ}$ (10). A step scan technique was used at a step width of $0.005^{\circ}$ in the $2 \theta$-range from $20^{\circ}$ to $80^{\circ}$ for $\lambda=1.2 \AA, 0.005^{\circ}$ in the $2 \theta$-range from $20^{\circ}$ to $100^{\circ}$ for $\lambda=1.54 \AA$, and $0.004^{\circ}$ in the $2 \theta$-range from $20^{\circ}$ to $100^{\circ}$ for $\lambda=1.6 \AA$.

## STRUCTURE ANALYSIS

## Space-Group Assignment and Rietveld Refinements

Observed diffraction patterns were resolved into individual peaks using the computer program WPPF for the whole-powder-pattern-decomposition method (11). These peaks could be indexed by assuming an orthorhombic cell $(a \approx 12 \AA, b \approx 22 \AA$ and $c \approx 8 \AA, Z=2)$ with the doubled $c$ axis length of the reported basic cell (2). Observed systematic absences of reflections were consistent with those assigned by space groups $P b n 2_{1}$ and $\operatorname{Pbnm}$. No further unindexed reflection could be observed. Parts of the profile fitting results are shown in Fig. 1.


FIG. 1. Powder diffraction patterns of the $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}$ at $\lambda=1.2 \AA$ (detail). Dots, observations; solid lines, profiles calculated by program WPPF for the whole-powder-pattern-decomposition. Vertical arrows with indices point to superstructure reflections.

Structure parameters were refined by the Rietveld method using the latest version of the computer program PFLS (12) on the assumption of the centrosymmetric space group Pbnm, which follows from successful single crystal structure refinements by (6,7). In the first, profile parameters were varied. They were a scale factor, parameters of the fifth-degree polynomial background function, the unit cell, the peak-shift correction for $2 \theta$-zero point, the pseudoVoigt function (13), the Caglioti et al. formula (14), the correction for preferred orientation (15), and overall temperature parameter. After obtaining their convergence, structural parameters were varied. The structure has three types of cation sites, which are designated by using symbols Ti, $\mathrm{A}_{1}$, and $\mathrm{A}_{2}$ for $\mathrm{TiO}_{6}$ octahedral sites, tetragonal tunnel sites, and pentagonal tunnel sites, respectively. Since there was parameter correlation between the thermal displacement parameters and site occupancy parameters, atoms were placed into groups of four in refining thermal displacement parameters. One group consists of Ti atoms, the second $\mathrm{Ba} / \mathrm{Sm}$ atoms at the $\mathrm{A}_{1}$ sites, the third Ba atoms at the $A_{2}$ sites, and the fourth oxygen atoms. Common thermal displacement parameters were assigned to respective groups. The Ti and oxygen sites were assumed to be fully occupied. Refinements of site occupancy parameters for the $\mathrm{A}_{1}$ and $\mathrm{A}_{2}$ sites will be described in next sections.

In these refinements, the weight function $w_{i}=1 / Y_{o i}^{e}\left(Y_{o i}\right.$ $=$ observed profile intensity and $e$ is the adjustable parameter) was optimized so as to obtain a unimodal distribution of weighted residuals (16). All the atoms were assumed to be fully ionized. Scattering factors for $\mathrm{Ti}^{4+}, \mathrm{Ba}^{2+}$, and $\mathrm{Sm}^{3+}$ were taken from (17) and that for $\mathrm{O}^{2-}$ from (18). Anomalous dispersion terms at particular wavelengths were taken from (19). The constraint by the chemical composition was applied except as noted. Initial positional parameters for the refinement were taken from (6) for BST71. Other refinement conditions are given in Table 1. Refined unit cell parameters are given in Table 2.

## Site Occupancy Refinements for BST30 and BST50

Samples of BST30 and BST50 have 5.1 and 4.5 Ba atoms over the four $\mathrm{A}_{2}$ sites, respectively. Thus these excess Ba were expected to coexist with Sm at the $\mathrm{A}_{1}$ sites. The present samples will have also a certain amount of cation vacancy at the $\mathrm{A}_{1}$ sites. Therefore, we have tried to determine the distribution of vacancies over these $\mathrm{A}_{1}$ sites first.
If the structure is centrosymmetric, an imaginary part of the dispersion term will have a minor contribution to the structure factor. On the other hand, a sum of two real parts, Thomson scattering factor and a real part of the anomalous scattering factor, for Sm will become similar to that for Ba when the intensity data measured with the wavelength of $1.6 \AA$ are used. In this case, two kinds of different atoms can be treated as one kind of atom, when only the total

TABLE 1
Conditions for Rietveld Structure Refinement for $\mathrm{Ba}_{6-x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}$

| Space group | Pbnm (No. 62), $Z=2$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Profile shape | Split-type pseudo-Voigt function |  |  |  |
| Background | 5th-degree polynomial function |  |  |  |
| Peak shift | $2 \theta$-zero point |  |  |  |
| Preferred orientation func | n Symmetrized harmonics expansion with five coefficients |  |  |  |
| Weighting scheme | $w_{i}=1 / Y_{\text {o } i}^{e}$ |  |  |  |
| $x=$ | 0.3 | 0.5 | 0.67 | 0.71 |
| $\lambda=1.60 \AA$ |  |  |  |  |
| $2 \theta$ Range analyzed ( ${ }^{\circ}$ ) | $20 \leq 2 \theta \leq 100$ |  |  |  |
| No. observations | 20001 | 20001 | $16001{ }^{\text {a }}$ | 20001 |
| No. of flections | 1051 | 1049 | $1164{ }^{\text {a }}$ | 1046 |
| Parameters refined (final) | 101 | 102 | 102 | 104 |
| $e$ in weight function | 1.8 | 1.8 | 1.4 | 1.6 |
| $R_{\text {p }}$ | 0.11 | 0.09 | 0.12 | 0.10 |
| $R_{\text {wp }}$ | 0.15 | 0.13 | 0.18 | 0.14 |
| $\lambda=1.20 \AA$ |  |  |  |  |
| $2 \theta$ Range analyzed ( ${ }^{\circ}$ ) | $20 \leq 2 \theta \leq 80$ |  |  |  |
| No. of observations | 12001 | 12001 | 12001 | 12001 |
| No. of reflections | 1432 | 1423 | 1417 | 1415 |
| Parameters refined (final) | 100 | 100 | 103 | 104 |
| $e$ in weight function | 2.3 | 2.4 | 2.2 | 2.2 |
| $R_{\text {p }}$ | 0.08 | 0.07 | 0.08 | 0.07 |
| $R_{\text {wp }}$ | 0.09 | 0.08 | 0.09 | 0.08 |

${ }^{a}$ Data measured at step width of $0.005^{\circ}$ and $\lambda=1.54(\AA)$, see text.
scattering powers are taken into account, in the determination of vacancies at the $\mathrm{A}_{1}$ sites using a $1.6-\AA$ data set. In the least-squares calculations at this stage, the same occupancy ratio of $\mathrm{Ba} / \mathrm{Sm}$ was assigned to the atoms at the five $\mathrm{A}_{1}$ sites. The occupancy parameters for the $\mathrm{A}_{1}(5)$ site became slightly larger than 1 , and thus it was kept fixed at 1 in further calculation. Parameters were converged after several iterations of the least-squares cycles. A result of the determination of vacancy distribution is presented in Table 3. It showed that the vacancies are distributed over the $\mathrm{A}_{1}(1)$ sites by 11 to $17 \%$ and over the $\mathrm{A}_{1}(3)$ and $\mathrm{A}_{1}(4)$ sites in small amounts. The $R_{\mathrm{p}}$ and $R_{\mathrm{wp}}$ factors were 0.11 and 0.15 for BST30 and 0.09 and 0.13 for BST50, respectively, at this stage.

TABLE 2
The Unit-Cell Parameters for $\mathbf{B a}_{6-3 x} \mathbf{S m}_{8+2 x} \mathbf{T i}_{18} \mathbf{O}_{54}$

| Composition, $x$ | 0.3 | 0.5 | 0.67 | 0.71 |
| :---: | :---: | :---: | :---: | :---: |
| Cell dimensions ( $\AA$ ) |  |  |  |  |
| $a=$ | 12.1715(5) | 12.1568(1) | 12.1472(1) | 12.1452(1) |
| $b=$ | $22.3772(3)$ | 22.3253(2) | 22.2972(2) | 22.3029(2) |
| $c=$ | 7.67523(9) | 7.66301(7) | 7.65338(6) | 7.65007(6) |
| Volume ( ${ }^{\text { }}$ ) | 2090.45(4) | 2079.78(3) | 2072.91(3) | 2072.20(3) |

TABLE 3
Site Occupancies and Their E.s.d.s for Tetragonal and Pentagonal Sites

| Site | Atom | $x=0.3$ | $x=0.5$ | $x=0.67$ | $x=0.71$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\lambda=1.6$ ( A ) |  |  |  |  |  |
| $\mathrm{A}_{1}(1)$ |  | 0.89(1) | 0.833(8) |  |  |
| $\mathrm{A}_{1}(2)$ |  | 1.00(1) | 0.994(8) |  |  |
| $\mathrm{A}_{1}(3)$ |  | $0.989(8)$ | 0.954(7) |  |  |
| $\mathrm{A}_{1}(4)$ |  | 0.97(1) | 0.970(9) |  |  |
| $\mathrm{A}_{1}(5)$ |  | 1 | 1 |  |  |
| $\lambda=1.2$ ( $\AA$ ) |  |  |  |  |  |
| $\mathrm{A}_{1}(1)$ | Sm | 0.68(6) | 0.72(4) | 0.791(6) | 0.803(5) |
|  | Ba | 0.21 | 0.12 |  |  |
| $\mathrm{A}_{1}(2)$ | Sm | $1.00{ }^{\text {a }}$ | $0.994^{a}$ | $0.982(7)$ | $0.989(5)$ |
| $\mathrm{A}_{1}(3)$ | Sm | $0.65(4)$ | $0.82(4)$ | 0.910 (6) | 0.919(5) |
|  | Ba | 0.34 | 0.13 |  |  |
| $\mathrm{A}_{1}(4)$ | Sm | $0.97{ }^{\text {a }}$ | $0.970^{a}$ | 0.993(7) | 0.990(6) |
| $\mathrm{A}_{1}(5)$ | Sm | $1^{a}$ | $1^{a}$ | 0.991(6) | 1 |
| $\mathrm{A}_{2}(1)$ | Ba | 1 | 1 | 1 | 0.988(7) |
| $\mathrm{A}_{2}(2)$ | Ba | 1 | 1 | 1 | 0.952(7) |

[^1]After fixing the amount of vacancy, the distributions of Sm and Ba over the five $\mathrm{A}_{1}$ sites could be determined by using intensity data measured with the wavelength of $1.2 \AA$. The occupancy parameter of Ba at the $\mathrm{A}_{1}(2), \mathrm{A}_{1}(4)$, and $A_{1}(5)$ sites became slightly negative, and then they were kept fixed at zero in further calculation. All parameters converged and the final $R_{\mathrm{p}}$ and $R_{\mathrm{wp}}$ factors were 0.08 and 0.09 for BST30 and 0.07 and 0.08 for BST50, respectively. Site occupancy parameters, thus obtained, are presented in Table 3. Other positional parameters and thermal displacement parameters are given in Table 4. Selected interatomic distances are given in Tables 5 and 6. A fitting result in Rietveld refinement for BST30 is given in Fig. 2.

## Site Occupancy Refinement for BST67 and BST71

Samples of BST71 have vacancies at both $\mathrm{A}_{1}$ and $\mathrm{A}_{2}$ sites and samples of BST67 have vacancies at $\mathrm{A}_{1}$ sites. In the first, the site occupancy parameters of Sm and Ba at respective sites were varied independently. In this case, the constraint by the chemical composition was not applied. Two sets of refinements using the two wavelength data sets for 1.2 and $1.6 \AA$ ( $1.54 \AA$ for BST67) resulted in virtually the same result, indicating no exchange of Ba at the $\mathrm{A}_{2}$ sites with Sm atoms at the $A_{1}$ site and vice versa.

Second, the site occupancy parameters were refined. The parameters became larger than 1 for the $\mathrm{A}_{1}(5)$ site in BST71. Thus it was kept fixed at 1 in further calculation. The final $R_{\mathrm{p}}$ and $R_{\mathrm{wp}}$ factors after the least-squares calculations were 0.08 and 0.09 for BST67 and 0.07 and 0.08 for BST71,

TABLE 4
Refined Positional and Isotropic Thermal Displacement Parameters and Their E.s.d.s for $\mathbf{B a}_{6-3 x} \mathbf{S m}_{8+2 x} \mathbf{T i}_{18} \mathbf{O}_{54}$

|  | $x$ | $y$ | $z$ | $B_{\text {iso }}\left(\AA^{2}\right)^{a}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Ba}_{5.1} \mathrm{Sm}_{8.6} \mathrm{Ti}_{18} \mathrm{O}_{54}(\mathrm{BST} 30 x=0.3)$ |  |  |  |  |
| $\mathrm{Ti}(1)$ | 0.0 | 0.0 | 0.0 | 0.55 (4) |
| Ti(2) | 0.1994(4) | 0.4336(2) | 0.001(1) | 0.55 |
| Ti(3) | 0.3977(4) | 0.1069(2) | $-0.000(1)$ | 0.55 |
| $\mathrm{Ti}(4)$ | 0.1187(4) | 0.1641(2) | -0.009(1) | 0.55 |
| Ti(5) | 0.3400(4) | 0.2604(2) | -0.003(1) | 0.55 |
| $\mathrm{A}_{1}(1)$ | 0.1926(2) | 0.0462(1) | 1/4 | 0.59(3) |
| $\mathrm{A}_{1}(2)$ | 0.7053(2) | $0.4486(1)$ | 1/4 | 0.59 |
| $\mathrm{A}_{1}(3)$ | 1.0008(3) | 0.4948(1) | 1/4 | 0.59 |
| $\mathrm{A}_{1}(4)$ | 0.4050(3) | 0.3776(1) | 1/4 | 0.59 |
| $\mathrm{A}_{1}(5)$ | 0.9091(3) | 0.1234(1) | 1/4 | 0.59 |
| $\mathrm{A}_{2}(1)$ | 0.0866(2) | 0.3013(1) | 1/4 | 0.65(4) |
| $\mathrm{A}_{2}(2)$ | 0.5966(2) | 0.1870(1) | 1/4 | 0.65 |
| $\mathrm{O}(1)$ | 0.093(2) | 0.167(1) | 1/4 | 0.55(9) |
| $\mathrm{O}(2)$ | 0.595(2) | 0.363(1) | 1/4 | 0.55 |
| $\mathrm{O}(3)$ | 0.423(1) | 0.1932(6) | 0.013(4) | 0.55 |
| $\mathrm{O}(4)$ | 0.688(1) | 0.2621(6) | -0.016(3) | 0.55 |
| $\mathrm{O}(5)$ | 0.336(2) | 0.275(1) | 1/4 | 0.55 |
| $\mathrm{O}(6)$ | 0.811(2) | 0.222(1) | 1/4 | 0.55 |
| $\mathrm{O}(7)$ | 0.377(1) | 0.0174(6) | 0.003(3) | 0.55 |
| $\mathrm{O}(8)$ | 0.215(2) | 0.443(1) | 1/4 | 0.55 |
| $\mathrm{O}(9)$ | 0.679(2) | 0.057(1) | 1/4 | 0.55 |
| $\mathrm{O}(10)$ | 0.242(1) | 0.1095(6) | 0.028(2) | 0.55 |
| $\mathrm{O}(11)$ | 0.479(2) | 0.482(1) | 1/4 | 0.55 |
| $\mathrm{O}(12)$ | 0.039(1) | 0.0808(7) | 0.060(2) | 0.55 |
| $\mathrm{O}(13)$ | 0.759(1) | 0.1409(7) | 0.037(2) | 0.55 |
| $\mathrm{O}(14)$ | 0.848(1) | 0.0197(7) | 0.051(2) | 0.55 |
| $\mathrm{O}(15)$ | 0.055(1) | 0.4071(6) | 0.045(2) | 0.55 |
| $\mathrm{O}(16)$ | 0.457(1) | 0.3184(6) | 0.021(3) | 0.55 |
| $\mathrm{O}(17)$ | 0.432(2) | 0.0993(9) | 1/4 | 0.55 |
| $\mathrm{O}(18)$ | 0.877(2) | 0.409(1) | 1/4 | 0.55 |


| $\mathrm{Ba}_{4.5} \mathrm{Sm}_{9.0} \mathrm{Ti}_{18} \mathrm{O}_{54}(\mathrm{BST} 50 x=0.5)$ |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| $\mathrm{Ti}(1)$ | 0.0 | 0.0 | 0.0 | $0.53(3)$ |
| $\mathrm{Ti}(2)$ | $0.1994(3)$ | $0.4339(1)$ | $0.0042(8)$ | 0.53 |
| $\mathrm{Ti}(3)$ | $0.3980(3)$ | $0.1068(1)$ | $0.0078(7)$ | 0.53 |
| $\mathrm{Ti}(4)$ | $0.1176(3)$ | $0.1632(2)$ | $0.0002(9)$ | 0.53 |
| $\mathrm{Ti}(5)$ | $0.3397(3)$ | $0.2612(1)$ | $0.0002(9)$ | 0.53 |
| $\mathrm{~A}_{1}(1)$ | $0.1930(2)$ | $0.0452(1)$ | $1 / 4$ | $0.63(3)$ |
| $\mathrm{A}_{1}(2)$ | $0.7047(2)$ | $0.44887(8)$ | $1 / 4$ | 0.63 |
| $\mathrm{~A}_{1}(3)$ | $0.9999(2)$ | $0.4946(1)$ | $1 / 4$ | 0.63 |
| $\mathrm{~A}_{1}(4)$ | $0.4043(2)$ | $0.37745(9)$ | $1 / 4$ | 0.63 |
| $\mathrm{~A}_{1}(5)$ | $0.9095(2)$ | $0.12405(8)$ | $1 / 4$ | 0.63 |
| $\mathrm{~A}_{2}(1)$ | $0.0851(2)$ | $0.30026(9)$ | $1 / 4$ | $0.54(2)$ |
| $\mathrm{A}_{2}(2)$ | $0.5957(2)$ | $0.18673(8)$ | $1 / 4$ | 0.54 |
| $\mathrm{O}(1)$ | $0.104(2)$ | $0.1746(9)$ | $1 / 4$ | $1.11(8)$ |
| $\mathrm{O}(2)$ | $0.592(2)$ | $0.3578(9)$ | $1 / 4$ | 1.11 |
| $\mathrm{O}(3)$ | $0.421(1)$ | $0.1934(5)$ | $0.005(3)$ | 1.11 |
| $\mathrm{O}(4)$ | $0.6862(9)$ | $0.2638(6)$ | $0.005(3)$ | 1.11 |
| $\mathrm{O}(5)$ | $0.311(2)$ | $0.2751(9)$ | $1 / 4$ | 1.11 |
| $\mathrm{O}(6)$ | $0.845(2)$ | $0.2182(9)$ | $1 / 4$ | 1.11 |
| $\mathrm{O}(7)$ | $0.380(1)$ | $0.01615)$ | $-0.004(2)$ | 1.11 |
| $\mathrm{O}(8)$ | $0.225(2)$ | $0.4424(8)$ | $1 / 4$ | 1.11 |
| $\mathrm{O}(9)$ | $0.675(2)$ | $0.0524(9)$ | $1 / 4$ | 1.11 |
| $\mathrm{O}(10)$ | $0.244(1)$ | $0.1106(5)$ | $0.013(2)$ | 1.11 |
| $\mathrm{O}(11)$ | $0.478(2)$ | $0.4839(8)$ | $1 / 4$ | 1.11 |
| $\mathrm{O}(12)$ | $0.037(1)$ | $0.0809(6)$ | $0.049(2)$ | 1.11 |

TABLE 4-Continued

|  | $x$ | $y$ | $z$ | $B_{\text {iso }}\left(\AA^{2}\right)^{a}$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Ba}_{4.5} \mathrm{Sm}_{9.0} \mathrm{Ti}_{18} \mathrm{O}_{54}($ BST50 $x=0.5)$ |  |  |  |  |
| $\mathrm{O}(13)$ | 0.762(1) | 0.1380 (5) | 0.029(2) | 1.11 |
| $\mathrm{O}(14)$ | 0.845(1) | 0.0194(6) | 0.047(2) | 1.11 |
| $\mathrm{O}(15)$ | 0.058(1) | $0.4062(5)$ | 0.045(2) | 1.11 |
| $\mathrm{O}(16)$ | 0.460(1) | 0.3172(5) | 0.018(3) | 1.11 |
| $\mathrm{O}(17)$ | 0.428(2) | 0.1010(8) | 1/4 | 1.11 |
| $\mathrm{O}(18)$ | 0.878(2) | 0.4058(9) | 1/4 | 1.11 |
| $\mathrm{Ba}_{3.99} \mathrm{Sm}_{9.34} \mathrm{Ti}_{18} \mathrm{O}_{54}(\mathrm{BST} 67 x=0.67)$ |  |  |  |  |
| $\mathrm{Ti}(1)$ | 0.0 | 0.0 | 0.0 | 0.41(4) |
| $\mathrm{Ti}(2)$ | 0.1998(3) | 0.4339(2) | 0.0050(8) | 0.41 |
| Ti(3) | 0.3971(3) | 0.1062(1) | 0.0108(7) | 0.41 |
| $\mathrm{Ti}(4)$ | 0.1168(3) | 0.1634(2) | 0.0012(8) | 0.41 |
| $\mathrm{Ti}(5)$ | 0.3393(3) | 0.2618(2) | 0.0025(9) | 0.41 |
| $\mathrm{A}_{1}(1)$ | $0.1935(2)$ | $0.0446(1)$ | 1/4 | 0.65(3) |
| $\mathrm{A}_{1}(2)$ | $0.7047(2)$ | $0.44894(9)$ | 1/4 | 0.65 |
| $\mathrm{A}_{1}(3)$ | 0.9991(2) | 0.4944(1) | 1/4 | 0.65 |
| $\mathrm{A}_{1}(4)$ | $0.4046(2)$ | $0.37708(9)$ | 1/4 | 0.65 |
| $\mathrm{A}_{1}(5)$ | $0.9089(2)$ | 0.12402(9) | 1/4 | 0.65 |
| $\mathrm{A}_{2}(1)$ | $0.0846(2)$ | $0.29986(9)$ | 1/4 | $0.55(4)$ |
| $\mathrm{A}_{2}(2)$ | 0.5960(2) | $0.18715(9)$ | 1/4 | 0.55 |
| $\mathrm{O}(1)$ | 0.102(2) | 0.1770(9) | 1/4 | 1.3(1) |
| $\mathrm{O}(2)$ | 0.595(2) | 0.3565(9) | 1/4 | 1.3 |
| $\mathrm{O}(3)$ | 0.419(1) | 0.1951(6) | 0.007(3) | 1.3 |
| $\mathrm{O}(4)$ | 0.687(1) | 0.2630(6) | 0.014(3) | 1.3 |
| $\mathrm{O}(5)$ | 0.309(2) | 0.2734(9) | 1/4 | 1.3 |
| $\mathrm{O}(6)$ | 0.845(2) | 0.215(1) | 1/4 | 1.3 |
| $\mathrm{O}(7)$ | 0.378(1) | 0.0151(6) | 0.012(2) | 1.3 |
| $\mathrm{O}(8)$ | 0.227(2) | 0.4442(9) | 1/4 | 1.3 |
| $\mathrm{O}(9)$ | 0.671(2) | 0.054(1) | 1/4 | 1.3 |
| O(10) | 0.242(1) | 0.1113(6) | 0.016(2) | 1.3 |
| $\mathrm{O}(11)$ | 0.476(2) | 0.4841(9) | 1/4 | 1.3 |
| $\mathrm{O}(12)$ | 0.037(1) | 0.0818(6) | 0.042(2) | 1.3 |
| $\mathrm{O}(13)$ | 0.767(1) | 0.1378(6) | 0.026(2) | 1.3 |
| $\mathrm{O}(14)$ | 0.849(1) | 0.0214(7) | 0.047(2) | 1.3 |
| $\mathrm{O}(15)$ | 0.059(1) | 0.4093(6) | 0.047(2) | 1.3 |
| $\mathrm{O}(16)$ | 0.461(1) | 0.3154(6) | 0.013(3) | 1.3 |
| $\mathrm{O}(17)$ | 0.427(2) | 0.1016(8) | 1/4 | 1.3 |
| $\mathrm{O}(18)$ | 0.878(2) | 0.413(1) | $1 / 4$ | 1.3 |
| $\mathrm{Ba}_{3.87} \mathrm{Sm}_{9.42} \mathrm{Ti}_{18} \mathrm{O}_{54}($ BST71 $x=0.71)$ |  |  |  |  |
| $\mathrm{Ti}(1)$ | 0.0 | 0.0 | 0.0 | 0.71(3) |
| Ti(2) | 0.1992(3) | 0.4343(1) | $0.0025(7)$ | 0.71 |
| $\mathrm{Ti}(3)$ | 0.3981(3) | 0.1069(1) | 0.0080(7) | 0.71 |
| Ti(4) | 0.1172(3) | 0.1630(2) | 0.0010(8) | 0.71 |
| Ti(5) | 0.3388(3) | 0.2616(2) | 0.0006(8) | 0.71 |
| $\mathrm{A}_{1}(1)$ | 0.1936(2) | 0.0449(1) | 1/4 | 0.63(2) |
| $\mathrm{A}_{1}(2)$ | $0.7047(2)$ | 0.44900 (8) | 1/4 | 0.63 |
| $\mathrm{A}_{1}(3)$ | $0.9988(2)$ | 0.4942(1) | 1/4 | 0.63 |
| $\mathrm{A}_{1}(4)$ | $0.4042(2)$ | $0.37696(8)$ | 1/4 | 0.63 |
| $\mathrm{A}_{1}(5)$ | $0.9095(2)$ | $0.12400(8)$ | 1/4 | 0.63 |
| $\mathrm{A}_{2}(1)$ | $0.0845(2)$ | $0.30012(9)$ | 1/4 | 0.54(4) |
| $\mathrm{A}_{2}(2)$ | 0.5958(2) | $0.18716(9)$ | 1/4 | 0.54 |
| $\mathrm{O}(1)$ | 0.100(2) | 0.1766 (9) | 1/4 | 1.41(8) |
| $\mathrm{O}(2)$ | 0.591(2) | 0.3584(9) | 1/4 | 1.41 |
| $\mathrm{O}(3)$ | 0.419(1) | 0.1929(6) | 0.006(3) | 1.41 |
| $\mathrm{O}(4)$ | 0.6871(9) | 0.2637(6) | 0.012(2) | 1.41 |
| $\mathrm{O}(5)$ | 0.309(2) | 0.2760 (9) | 1/4 | 1.41 |
| $\mathrm{O}(6)$ | 0.853(2) | $0.2160(9)$ | 1/4 | 1.41 |
| $\mathrm{O}(7)$ | 0.3752(9) | 0.0161(5) | 0.003(2) | 1.41 |

TABLE 4-Continued

|  | $x$ | $y$ | $z$ | $B_{\text {iso }}\left(\AA^{2}\right)^{a}$ |
| :--- | :---: | :--- | :--- | :--- |
| $\mathrm{Ba}_{3.87} \mathrm{Sm}_{9.42} \mathrm{Ti}_{18} \mathrm{O}_{54}(\mathrm{BST71} x=0.71)$ |  |  |  |  |
| $\mathrm{O}(8)$ | $0.228(2)$ | $0.4424(8)$ | $1 / 4$ | 1.41 |
| $\mathrm{O}(9)$ | $0.670(2)$ | $0.0532(9)$ | $1 / 4$ | 1.41 |
| $\mathrm{O}(10)$ | $0.242(1)$ | $0.1089(6)$ | $0.019(2)$ | 1.41 |
| $\mathrm{O}(11)$ | $0.477(2)$ | $0.4840(8)$ | $1 / 4$ | 1.41 |
| $\mathrm{O}(12)$ | $0.037(1)$ | $0.0807(6)$ | $0.042(2)$ | 1.41 |
| $\mathrm{O}(13)$ | $0.767(1)$ | $0.1388(5)$ | $0.026(2)$ | 1.41 |
| $\mathrm{O}(14)$ | $0.848(1)$ | $0.0195(6)$ | $0.045(2)$ | 1.41 |
| $\mathrm{O}(15)$ | $0.058(1)$ | $0.4071(5)$ | $0.049(2)$ | 1.41 |
| $\mathrm{O}(16)$ | $0.461(1)$ | $0.3170(5)$ | $0.011(3)$ | 1.41 |
| $\mathrm{O}(17)$ | $0.426(2)$ | $0.1012(8)$ | $1 / 4$ | 1.41 |
| $\mathrm{O}(18)$ | $0.880(2)$ | $0.4077(9)$ | $1 / 4$ | 1.41 |

${ }^{a}$ Common $B_{\text {iso }} \mathrm{s}$ were used for each $\mathrm{Ti}-, \mathrm{A}_{1}, \mathrm{~A}_{2}$-, and O - site atoms.
respectively. Final atomic parameters are given in Tables 3 and 4. Selected interatomic distances are given in Tables 5 and 6 .

TABLE 5
Selected Interatomic Distances $(\AA)$ and Their E.s.d.s at
the $\mathrm{TiO}_{6}$ Octahedra of $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathbf{0}_{54}$

|  | $x=0.3$ | $x=0.5$ | $x=0.67$ | $x=0.71$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Ti}(1)-\mathrm{O}(11) \quad 2 \times$ | $1.976(5)$ | 1.967(4) | 1.967(5) | 1.965(4) |
| $\mathrm{Ti}(1)-\mathrm{O}(12) \quad 2 \times$ | 1.93(2) | 1.90(1) | 1.91(1) | 1.88(1) |
| $\mathrm{Ti}(1)-\mathrm{O}(13) \quad 2 \times$ | 1.94(2) | 1.96(1) | 1.93(1) | 1.92(1) |
| Mean value | 1.95(1) | 1.94(1) | 1.94(1) | 1.92(1) |
| $\mathrm{Ti}(2)-\mathrm{O}(7)$ | 2.10(1) | 2.07(1) | 2.04(1) | 2.03(1) |
| $\mathrm{Ti}(2)-\mathrm{O}(8)$ | 1.933(9) | 1.920(7) | 1.917(7) | 1.933(7) |
| $\mathrm{Ti}(2)-\mathrm{O}(9)$ | 1.952(9) | 1.993(8) | 2.000(7) | 1.984(7) |
| $\mathrm{Ti}(2)-\mathrm{O}(13)$ | 1.84(2) | 1.79(1) | 1.81(1) | 1.84(1) |
| $\mathrm{Ti}(2)-\mathrm{O}(14)$ | 2.13(2) | 2.10(1) | 2.10(1) | 2.11(1) |
| $\mathrm{Ti}(2)-\mathrm{O}(15)$ | 1.88(2) | 1.85(1) | 1.83(1) | 1.86(1) |
| Mean value | 1.97(1) | $1.95(1)$ | $1.95(1)$ | 1.96(1) |
| $\mathrm{Ti}(3)-\mathrm{O}(3)$ | 1.96(1) | 1.96(1) | 2.00(1) | 1.93(1) |
| $\mathrm{Ti}(3)-\mathrm{O}(7)$ | 2.02(1) | 2.04(1) | 2.05(1) | 2.05 (1) |
| $\mathrm{Ti}(3)-\mathrm{O}(10)$ | 1.91(2) | 1.87(1) | 1.89(1) | 1.90(1) |
| $\mathrm{Ti}(3)-\mathrm{O}(15)$ | 1.97(2) | 2.01(1) | 2.04(1) | 2.01(1) |
| $\mathrm{Ti}(3)-\mathrm{O}(17)$ | 1.973(9) | 1.895(7) | 1.869(7) | 1.886(6) |
| $\mathrm{Ti}(3)-\mathrm{O}(18)$ | 1.964(9) | 2.011(7) | 2.053(7) | 2.013(7) |
| Mean value | 1.97(1) | 1.96(1) | 1.98(1) | 1.96(1) |
| $\mathrm{Ti}(4)-\mathrm{O}(1)$ | 2.011(9) | 1.939(7) | 1.937(8) | 1.939(7) |
| $\mathrm{Ti}(4)-\mathrm{O}(2)$ | 1.97(1) | 1.997(9) | 1.991(9) | 2.005(9) |
| $\mathrm{Ti}(4)-\mathrm{O}(3)$ | 1.86(1) | 1.83(1) | 1.85(1) | 1.84(1) |
| $\mathrm{Ti}(4)-\mathrm{O}(10)$ | 1.96(2) | 1.94(1) | 1.91(1) | 1.94(1) |
| $\mathrm{Ti}(4)-\mathrm{O}(12)$ | 2.17(2) | 2.12(1) | 2.09(1) | 2.10(1) |
| $\mathrm{Ti}(4)-\mathrm{O}(16)$ | 2.01(1) | 1.97(1) | $1.95(1)$ | 1.95 (1) |
| Mean value | 2.00(1) | 1.96(1) | 1.95(1) | 1.96(1) |
| $\mathrm{Ti}(5)-\mathrm{O}(3)$ | 1.82(1) | 1.81(1) | 1.78(1) | 1.81(1) |
| $\mathrm{Ti}(5)-\mathrm{O}(4)$ | 1.92(1) | 1.95(1) | 1.94(1) | 1.93(1) |
| $\mathrm{Ti}(5)-\mathrm{O}(5)$ | 1.97(1) | 1.970(9) | 1.946(8) | 1.968(8) |
| $\mathrm{Ti}(5)-\mathrm{O}(6)$ | 1.96(1) | 1.973(9) | 2.004(9) | 1.989(8) |
| $\mathrm{Ti}(5)-\mathrm{O}(13)$ | 2.43(2) | 2.45(1) | 2.42(1) | 2.40(1) |
| $\mathrm{Ti}(5)-\mathrm{O}(16)$ | 1.94(1) | 1.93(1) | 1.91(1) | 1.94(1) |
| Mean value | 2.01(1) | 2.01(1) | 2.00(1) | 2.01(1) |

TABLE 6
Selected Interatomic Distances ( $\AA$ ) and Their E.s.d.s at the Tetragonal and Pentagonal Sites of $\mathbf{B a}_{6-3 x} \mathbf{S m}_{8+2 x} \mathbf{T i}_{18} \mathbf{0}_{54}$

|  | $x=0.3$ | $x=0.5$ | $x=0.67$ | $x=0.71$ |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{A}_{1}(1)-\mathrm{O}(1)$ | 2.96(2) | 3.09(2) | 3.16(2) | 3.15(2) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(7) \quad 2 \times$ | 3.01(2) | $3.06(1)$ | 2.96(1) | 2.97(1) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(8)$ | 2.57(2) | 2.50(2) | 2.44(2) | 2.48(2) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(10) 2 \times$ | 2.29(2) | 2.41(2) | 2.40(2) | 2.35 (2) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(11)$ | 2.53(2) | 2.49(2) | 2.47(2) | 2.48(2) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(12) 2 \times$ | 2.49(2) | 2.57(1) | 2.62(1) | 2.61(1) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(14) 2 \times$ | 2.78(2) | 2.74(1) | 2.75(2) | 2.72(1) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(17)$ | 3.15 (2) | 3.12(2) | 3.11(2) | 3.08(2) |
| Mean value | 2.70(2) | 2.73(1) | 2.72(1) | 2.71(1) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(2)$ | 2.34(2) | 2.45(2) | 2.46(2) | 2.45(2) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(7) 2 \times$ | 2.95 (2) | 2.95(1) | 3.01(2) | 2.94(1) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(9)$ | 2.80(2) | 2.73(2) | 2.79(2) | 2.78(2) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(10) 2 \times$ | 2.54(2) | 2.46 (2) | 2.48(2) | 2.47(2) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(11)$ | 2.86(2) | 2.86(2) | 2.88(2) | 2.87(2) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(12) 2 \times$ | 3.19(2) | 3.14(1) | 3.10(1) | 3.10(1) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(14) 2 \times$ | 2.30(2) | 2.29(1) | 2.33(2) | 2.32(1) |
| $\mathrm{A}_{1}(2)-\mathrm{O}(18)$ | 2.28(2) | 2.32(2) | 2.26(2) | 2.31(2) |
| Mean value | 2.68(2) | 2.67(2) | 2.69(2) | 2.67(2) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(7) \quad 2 \times$ | 2.46 (2) | 2.48(2) | 2.40 (2) | 2.48(2) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(7)^{\prime} \quad 2 \times$ | 2.47(2) | 2.40 (2) | 2.50 (2) | 2.46(2) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(8)$ | 2.85(3) | 2.98(2) | 2.98(2) | 3.01(2) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(9)$ | 2.60(2) | 2.49(2) | 2.46 (2) | 2.44(2) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(15) 2 \times$ | 2.60(1) | 2.62(1) | 2.56(1) | 2.58(1) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(15)^{\prime} 2 \times$ | 3.22(2) | 3.24(1) | 3.21(1) | 3.25(1) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(17)$ | 2.48(2) | 2.53(2) | 2.55(2) | 2.56(2) |
| $\mathrm{A}_{1}(3)-\mathrm{O}(18)$ | 2.45(2) | 2.48(2) | 2.34(2) | 2.41(2) |
| Mean value | 2.66(2) | 2.66(2) | 2.64(2) | 2.66(2) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(2)$ | 2.33(3) | 2.33(2) | 2.36(2) | 2.30 (2) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(5)$ | 2.44(3) | 2.55(2) | 2.59(2) | 2.53(2) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(8)$ | 2.74(3) | 2.62(2) | 2.63(2) | 2.59(2) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(11)$ | 2.51(2) | 2.54(2) | 2.54(2) | 2.55(2) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(12) 2 \times$ | 3.03(2) | 2.95 (1) | 2.90(1) | 2.91(1) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(13) 2 \times$ | 2.86(2) | 2.77(2) | 2.71(2) | 2.71(2) |
| $\mathrm{A}_{1}(4)-\mathrm{O}(14) 2 \times$ | 3.33(2) | 3.32(1) | 3.28(2) | 3.30(1) |
| $\mathrm{A}_{1}(1)-\mathrm{O}(16) 2 \times$ | 2.29(2) | 2.33(2) | 2.38(2) | 2.37(2) |
| Mean value | 2.75 (2) | 2.73(2) | 2.72(2) | 2.72(2) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(1)$ | 2.43(3) | 2.62(2) | 2.63(2) | 2.60(2) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(6)$ | 2.52(2) | 2.24(2) | 2.16(2) | 2.16(2) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(9)$ | 3.16(2) | 3.27(2) | 3.28(2) | 3.31(2) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(11)$ | 3.44(2) | 3.41(2) | 3.42(2) | 3.41(2) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(12) 2 \times$ | $2.35(2)$ | 2.39(1) | 2.41(1) | 2.42(1) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(13) 2 \times$ | 2.48(2) | 2.49(2) | 2.45 (2) | 2.46(1) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(14) 2 \times$ | 2.87(2) | 2.91(1) | 2.86(1) | 2.91(2) |
| $\mathrm{A}_{1}(5)-\mathrm{O}(16) 2 \times$ | 2.52(2) | 2.51(2) | 2.50(2) | 2.47(2) |
| Mean value | 2.67(2) | 2.68(2) | 2.66 (2) | 2.67(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(1)$ | 3.02(2) | 2.81(2) | 2.75(2) | 2.76(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(3) 2 \times$ | 2.84(2) | 2.79(2) | 2.81(2) | 2.81(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(4) 2 \times$ | 2.60(2) | 2.72(2) | 2.75(2) | 2.75 (2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(5)$ | 3.09(3) | 2.80(2) | 2.79(2) | 2.78(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(6)$ | 3.79 (2) | 3.44(2) | 3.47(2) | 3.37(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(8)$ | 3.53(2) | 3.60(2) | 3.65(2) | 3.62(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(13) 2 \times$ | 3.30(2) | 3.33(1) | 3.36 (2) | $3.35(1)$ |
| $\mathrm{A}_{2}(1)-\mathrm{O}(15) 2 \times$ | 2.87(1) | 2.86(1) | 2.91(1) | 2.86(1) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(16) 2 \times$ | 3.74(2) | 3.66(2) | 3.59(2) | 3.61(2) |
| $\mathrm{A}_{2}(1)-\mathrm{O}(18)$ | 3.50(2) | 3.45 (2) | 3.55(2) | 3.46(2) |
| Mean value | 3.18(2) | 3.12(2) | 3.14(2) | 3.12(2) |

TABLE 6-Continued

|  | $x=0.3$ | $x=0.5$ | $x=0.67$ | $x=0.71$ |
| :--- | :---: | :---: | :---: | :---: |
| $\mathrm{~A}_{2}(2)-\mathrm{O}(2)$ | $3.94(2)$ | $3.81(2)$ | $3.78(2)$ | $3.82(2)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(3) 2 \times$ | $2.79(2)$ | $2.83(2)$ | $2.85(2)$ | $2.85(2)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(4) 2 \times$ | $2.87(2)$ | $2.77(2)$ | $2.71(2)$ | $2.73(2)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(5)$ | $3.74(3)$ | $3.99(2)$ | $3.98(2)$ | $4.00(2)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(6)$ | $2.73(2)$ | $3.11(2)$ | $3.09(2)$ | $3.20(2)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(9)$ | $3.07(3)$ | $3.15(2)$ | $3.11(2)$ | $3.12(2)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(13) 2 \times$ | $2.77(2)$ | $2.85(1)$ | $2.91(2)$ | $2.90(1)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(15) 2 \times$ | $3.13(2)$ | $3.10(1)$ | $3.16(1)$ | $3.14(1)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(16) 2 \times$ | $3.83(2)$ | $3.79(1)$ | $3.76(2)$ | $3.79(1)$ |
| $\mathrm{A}_{2}(2)-\mathrm{O}(17)$ | $2.80(2)$ | $2.80(2)$ | $2.80(2)$ | $2.82(2)$ |
| Mean value | $3.14(2)$ | $3.17(2)$ | $3.17(2)$ | $3.19(2)$ |

## RESULTS AND DISCUSSION

## Cation Distribution and Interatomic Distances

A projection of the crystal structure of BST30 on a (001) plane is shown in Fig. 3. As has been described above, present solid solutions have $\mathrm{TiO}_{6}$-framework structures with the five tetragonal and two pentagonal tunnels running parallel to the $c$ axis.
Results of the site occupancy refinements given in Table 3 showed that two of five tetragonal $\mathrm{A}_{1}$ sites $\left[\mathrm{A}_{1}(1)\right.$ and $\left.\mathrm{A}_{1}(3)\right]$ accommodate Ba in BST30 and BST50. Most of cation vacancies were also found at these two $A_{1}(1)$ and $A_{1}(3)$ sites in the samples examined. In particular, the $A_{1}(1)$ site commonly had smaller site occupancy than the others, and more than $2 / 3$ of total vacancies are concentrated at this site. The $\mathrm{A}_{1}(4)$ site have a little vacancy and the other two tetragonal sites $\left[\mathrm{A}_{1}(2)\right.$ and $\left.\mathrm{A}_{1}(5)\right]$ are virtually fully occupied by Sm . The total occupancies of Ba and Sm at the $\mathrm{A}_{1}(1)$ and $\mathrm{A}_{1}(3)$ sites have their minima with $x=0.67$, as expected from Eq. [1]. These minima are caused by (i) decreasing amount of Sm with decreasing $x$ and (ii) substitution of Ba at these sites in $x<0.67$. The $\mathrm{A}_{1}(1)$ and $\mathrm{A}_{1}(2)$ sites are crystallographically identical in the average structure. Therefore, this observation suggests that the formation of superstructure is due to the ordering of vacancy in the average structure. With $x=0.71$, cation vacancy was also found at $\mathrm{A}_{2}(2)$ site.

TABLE 7
Selected Bending Angles ( ${ }^{\circ}$ ) and Their E.s.d.s of the $\mathbf{T i O}_{6}$ Octahedra Joining along the $\boldsymbol{c}$ Axis

|  | $x=0.3$ | $x=0.5$ | $x=0.67$ | $x=0.71$ |
| :--- | :---: | :---: | :---: | :---: |
| $\mathrm{O}(11)-\mathrm{O}(11)^{\prime}-\mathrm{O}(11)$ | $152.3(6)$ | $153.8(5)$ | $153.3(6)$ | $153.5(6)$ |
| $\mathrm{O}(9)-\mathrm{O}(8)-\mathrm{O}(9)$ | $167.1(7)$ | $161.6(6)$ | $160.0(6)$ | $159.1(6)$ |
| $\mathrm{O}(18)-\mathrm{O}(17)-\mathrm{O}(18)$ | $159.6(7)$ | $161.4(6)$ | $160.1(6)$ | $162.4(6)$ |
| $\mathrm{O}(2)-\mathrm{O}(1)-\mathrm{O}(2)$ | $160.4(7)$ | $158.2(6)$ | $157.8(6)$ | $156.7(6)$ |
| $\mathrm{O}(6)-\mathrm{O}(5)-\mathrm{O}(6)$ | $170.9(7)$ | $166.8(6)$ | $164.7(7)$ | $163.2(6)$ |
| Mean value | $162.1(7)$ | $160.4(6)$ | $159.2(6)$ | $159.0(6)$ |



FIG. 2. Powder diffraction pattern of $\mathrm{Ba}_{5.1} \mathrm{Sm}_{8.6} \mathrm{Ti}_{18} \mathrm{O}_{54}$ and its fitting results by Rietveld refinement. (Top) Observations (dots) and calculated profile (solid line); (middle) difference between observations and calculated profile; (bottom) weighted difference ( $\times 5$ ).

As given in Table 6, $\mathrm{A}_{2}(1)-\mathrm{O}$ and $\mathrm{A}_{2}(2)-\mathrm{O}$ bond lengths remain unchanged. In spite of the substitution of Ba , averaged $\mathrm{A}_{1}(3)-\mathrm{O}$ bond lengths also remain unchanged. The $\mathrm{Ba}-\mathrm{O}$ distance calculated by the bond-valence scheme is $2.66 \AA(20)$, which is fairly close to, or slightly smaller than, the observed $\mathrm{A}_{1}-\mathrm{O}$ distances. In contrast with that, the $A_{1}(4)-O$ bond lengths appear to be steadily increased with decreasing occupancy at the $A_{1}(4)$ site. These observations suggest that these tetragonal cavities formed by $2 \times 2$ perov-skite-like blocks have an enough room for larger Ba and partial substitution of Ba has rather minor effect on $\mathrm{A}_{1}-\mathrm{O}$ bond distances.

## Lattice Deformation

The lattice modulation, which doubles the $c$ axis of the basic structure, can be illustrated as zig-zag bending of $\mathrm{TiO}_{6}$


FIG. 3. $\mathrm{TiO}_{6}$-framework structure of $\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54}$. Tetragonal and pentagonal site atoms were shown in white and shaded circles, respectively.
octahedra parallel to the $c$ axis (Fig. 4) (21). A bending angle of two $\mathrm{TiO}_{6}$ octahedra running parallel to the $c$ axis can be used as a measure of the lattice modulation. Observed bending angles given in Table 7 show that the mean value of these angles decreases with increasing $x$, indicating more lattice distortion with larger $x$ value. The increasing amount of cation vacancy at the $A_{1}(1)$ site, which is equivalent to the $A_{1}(2)$ site in the basic structure, will force to deform the framework. Even with partial substitution of Ba for Sm , the increase of total population at the $A_{1}(1)$ and $A_{1}(3)$ sites reduces an amplitude of this lattice modulation.


FIG. 4. Two $\mathrm{TiO}_{6}$ octahedra sharing an apex and arrayed parallel to the $c$ axis. $\mathrm{Ti}(1)$ is located at center of symmetry. Interatomic distance between two $\mathrm{O}(11)$ corresponds to the $c$-axis length of the cell.

$$
\mathrm{Ba}_{6-3 x} \mathrm{Sm}_{8+2 x} \mathrm{Ti}_{18} \mathrm{O}_{54} \text { SOLID SOLUTIONS }
$$

TABLE 8
Observed Relative Intensities (\%) of Some Superstructure Reflections

|  | Intensity |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| Bragg indices | $x=0.3$ | $x=0.5$ | $x=0.67$ | $x=0.71$ |
| 461 | 2.8 | 3.7 | 3.9 | 3.8 |
| 481 | 1.8 | 2.5 | 2.8 | 2.4 |

${ }^{a}$ Intensities at $\lambda=1.2 \AA$ were normalized with those of 125 reflection (most intense one).

Obtained by program WPPF for whole-powder-pattern decomposition.

Observed intensities of some superstructure reflections are presented in Table 8. In spite of the steady change of calculated superstructure intensities with $x$, the observed ones increased with $x$ in $x<0.67$ and then reduced with $x$ from 0.67 to 0.71 . This observation indicates that local lattice distortion, in addition to a long-range lattice modulation mentioned above, is possibly induced by the occupation of Ba and Sm at the same site in the composition range $x<2 / 3$ and the ordering of vacancy at $\mathrm{A}_{2}$ sites in $x>2 / 3$. This observation is in accordance with the observed physical properties, particularly of the quality factor having its maximum at $x=0.6$ (8).

## ACKNOWLEDGMENTS

Authors thank Mr. M. Imaeda at Nagoya Institute of Technology for useful discussions. This study has benefited from the use of facility at

Photon Factory, High Energy Accelerator Research Organization at Tsukuba, Japan.

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[^0]:    ${ }^{1}$ To whom correspondence should be addressed.

[^1]:    ${ }^{a}$ Obtained by refinements at $\lambda=1.6 \AA$

